In the use of this method as a setting method the main difficulty arises in selecting the reflexions to be brought into coincidence. This does not arise with irregular fragments of known unit cell (e.g. ground spheres), and the method may then prove superior to others. For example a colleague setting an irregular crystal of (?) face-centred cubic ferritungstite to [100] repeatedly converged on [111] by trial oscillation photographs. We had no difficulty in bringing two pairs of 111 reflexions into off-equatorial coincidence by this method, thus setting to the required axis. In some similar cases it may well happen that the predicted position of A in Fig. 1 lies outside the range of the arcs. The prediction will then be rather inaccurate owing to departures from the approximations above, but should suffice to indicate how the crystal should be remounted for a further triplet of trial rotation photographs. The indication of azimuth is likely to be more accurate than that of the inclination. It may be preferable to locate another known axis, accessible to the arcs, and derive the inclination from this.

Most workers use trial oscillation (or Laue) photographs for normal crystal setting, when using an irregular fragment. It is well known that recognizing badly misset layer lines is a knack, to be acquired by practice. The writer derived this method for general use before acquiring this knack, to study serendibite (Prior & Coomáraswámy, 1903; *cf.* Pertzev & Nikitina, 1959) available as type material in the form of rough irregular fragments thought to be triclinic. The above method was triumphantly successful at first attempt, setting a crystal on to an axis displaying equatorial symmetry on even-order, but not on odd-order layer lines, by using off-equatorial coincidences. The axis proved to be $[\overline{122}]$ of the reduced all-acute triclinic cell.

Subsequent use suggests that this success was partly accidental. The difficulty lies in properly selecting the reflexions to be brought into coincidence. Choice of off-equatorial coincidences if possible will favour setting to a symmetry axis if any exists. It seems likely that extending Fig. 1 to consider more than two reflexions, thus obtaining a consensus, offers best chance of success. The method used in these circumstances is simple and offers as much chance of quick success as trial oscillation photographs, but for general setting of irregular fragments, the method of Brooker & Nuffield, while more elaborate, is more certain. However, where the unit cell of the irregular fragment is known, the present method offers many advantages over other recommended photographic methods.

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The Decomposition of an Anisotropic Elastic Tensor

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The classical theory of invariants asserts that there exists a finite integrity basis whose elements are polynomials of strain components and are invariant under the group of transformation defining each symmetry class of a crystal. By constructing a strain energy function made up of the elements of an integrity basis for a certain symmetry class, we derive a tensor basis which spans the space of elastic constants for crystals of this symmetry class. Introducing systematically new elements of the integrity basis into the construction of the strain energy function, we construct five hierarchies of orthonormal tensor bases which span the space of the second-order elastic constants of all crystal systems. Any elastic tensor of rank four possessing certain crystallographic symmetry may be decomposed into a sum of tensors of increasing symmetry. From this representation of an anisotropic elastic tensor, the tensor of any given symmetry, not only the isotropic one, nearest the given tensor can be read off immediately. Bases which span the space of elastic constants of orders higher than the second may be computed in a similar manner. Such computations can be carried out by a computer. A FORMAC program of 7090/94 IBSYS has been written to obtain the elastic constants of the second and the third order for each class of a crystal.

1. Introduction

In an investigation of the physical properties of an anisotropic body, one sometimes begins with the corresponding properties of an isotropic body having the same geometry and proximal constitutive physical relations, and for which some knowledge may be obtainable with relative ease. It may then be possible to determine properties of the anisotropic body by the method of perturbation. Ways of defining and constructing the isotropic elastic tensor 'nearest' a given elastic tensor have been presented by Gazis, Tadjbakhsh & Toupin (1963). In this paper we construct orthonormal bases of tensors of rank four which span the space of elastic tensors possessing certain pointgroup symmetry of a crystal. The orientation of the Cartesian coordinates (x_1, x_2, x_3) conforms to the conventions in *IRE Standards on Piezoelectric Crystals* (Institute of Radio Engineers, 1949); namely,

Monoclinic $x_2||y,$ Tetragonal, trigonal and hexagonal $x_3||z, x_1||x,$ Orthorhombic and cubic $x_1||x, x_2||y, x_3||z,$

where (x, y, z) are the natural axes of symmetry of the crystal.

General procedures for the construction of linearly independent tensors of rank $2N, N=2,3,\ldots$ possessing given symmetry, are presented in § 2. By means of these tensors, orthonormal bases of tensors of given symmetry can be constructed and are given in § 3. The elements of the orthonormal bases of tensors of rank four are exhibited in both tensor and abbreviated matrix indices. The correspondence between the tensor indices and matrix indices is as follows:

Tensor indices:11223323,3231,1312,21Matrix indices:123456

For the elastic stiffness tensor, we set

 $c_{ijkl} = c_{MN}$ (*i*, *j*, *k*, *l* = 1, 2, 3 and *M*, *N* = 1, 2, ..., 6).

However, for the elastic compliance tensor s_{ijkl} , factors of 2 and 4 are introduced as follows:

 $s_{ijkl} = s_{MN}$ when both M and N are 1, 2 or 3, $2s_{ijkl} = s_{MN}$ when either M or N is 4, 5 or 6, $4s_{ijkl} = s_{MN}$ when both M and N are 4, 5 or 6.

Consequently, the matrix elements in § 3 must be multiplied by the factors 2 and 4 according to the above schemes.

To illustrate the method of decomposition, in § 4, the elastic stiffness tensor of quartz is decomposed into a sum of tensors of increasing symmetry. From this representation of an anisotropic elastic tensor, the tensor of any given symmetry, not only the isotropic one, nearest the given tensor can be read off immediately.

2. Invariant tensors

When a perfectly elastic crystal, initially stress-free, is deformed either isothermally or adiabatically to a final stressed state, the strain energy \overline{W} is a function of state. Furthermore, \overline{W} is invariant under the finite group of transformations, G, which defines the symmetry class of the crystal. For the purposes of this paper, it is assumed that \overline{W} is expressible as a polynomial in the strain components E_{ij} . Accordingly, if $||a_{ij}||$ is an element of G, and $\overline{E}_{ij} = a_{ik}a_{jl}E_{kl}$,* then it is required that

$$\overline{W}(\overline{E}_{ij}) = \overline{W}(E_{ij}) , \qquad (1)$$

for every $||a_{ij}||$ in G and all values of E_{ij} . A classical result of the theory of invariants (Weyl, 1946) is the existence of a finite integrity basis $\{I_1, I_2, \ldots, I_k\}$ such that every polynomial function satisfying (1) is expressible as a polynomial in the elements of the integrity basis. Each element I_n of an integrity basis is itself a polynomial in E_{ij} satisfying (1). For the case of an isotropic material, for example, an integrity basis has three elements. They are polynomials of the first, second and third degree in E_{ij} , respectively, and may be chosen as follows:

$$I = tr (E_{ij}) = E_{ii} = E_{11} + E_{22} + E_{33}$$

$$II = \frac{1}{2} [E_{ii}E_{jj} - E_{ij}E_{ij}]$$

$$= (E_{11}E_{22} + E_{22}E_{33} + E_{33}E_{11}) - (E_{12}^2 + E_{23}^2 + E_{31}^2)$$

$$III = det (E_{ij}) = \frac{1}{6} [E_{ii}E_{jj}E_{kk} - 3E_{ii}E_{jk}E_{kj} + 2E_{ij}E_{jk}E_{ki}]$$

$$= E_{11}E_{22}E_{33} + 2E_{12}E_{23}E_{31} - (E_{11}E_{23}^2 + E_{22}E_{31}^2 + E_{33}E_{12}^2)$$

$$(2)$$

Smith & Rivlin (1958) have determined the integrity basis for invariant functions of E_{ij} for each of the crystallographic point groups. Their results are summarized in Tables 1 and 2 for the purposes of the presentation of this paper. Table 1 gives the number of elements of an integrity-basis for each crystal class together with the number of the second- and third-order elastic constants. Table 2 gives some additional elements of polynomials of the first, second and third degree which are linearly independent of I, II and III of equations (2) as well as among themselves, together with the symmetry classes for which it is an invariant.

The second-order, third-order, ..., elastic constants are tensors of ranks four, six, ..., *etc.*, and are defined and denoted by

$$c_{ijkl} = \left\{ \frac{\partial^2 \bar{W}}{\partial E_{ij} \partial E_{kl}} \right\} ||E_{ij}|| = ||0|| ,$$

$$c_{ijklmn} = \left\{ \frac{\partial^3 \bar{W}}{\partial E_{ij} \partial E_{kl} \partial E_{mn}} \right\} ||E_{ij}|| = ||0|| ,$$

...., etc.
$$(3)$$

These quantities are symmetric in the following pairs of indices, (i,j), (k,l), (m,n) and (ij,kl), (ij,mn), (kl,mn). In particular, c_{ijkl} is called the elastic stiffness tensor. By choosing elements from Table 2 in addition to elements of (2), we shall form strain energy functions \overline{W} as polynomials of second and third degree in E_{ij} . Since polynomials of degree greater than three in the integrity basis do not contribute to the elastic tensors of ranks

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^{*} The summation convention on the double indices of tensors is understood throughout this paper.

		Number of eler integrity					n an		Num elastic c	Number of elastic constants			
Crystal systems	Class Schönflies	symbols International	1st degree	2nd degree	3rd degree	4th degree	5th degree	6th degree	2nd order	3rd order			
Triclinic	$\left\{\begin{array}{c} C_1\\ C_i\end{array}\right.$	$\frac{1}{1}$	6 6	0 0	0 0	0 0	0 0	0 0	21 21	56 56			
Monoclinic	$\left\{\begin{array}{c} C_2\\ C_s\\ C_{2h}\end{array}\right.$	2 m 2/m	4 4 4	3 3 3	0 0 0	0 0 0	0 0 0	0 0 0	13 13 13	32 32 32			
Orthorhombic	$\left\{\begin{array}{l} D_2\\ C_{2v}\\ D_{2h}\end{array}\right.$	222 mm2 mmm	3 3 3	3 3 3	1 1 1	0 0 0	0 0 0	0 0 0	9 9 9	20 20 20			
Tetragonal	$\left\{\begin{array}{l}C_4\\S_4\\C_{4h}\\D_4\\C_{4h}\\D_{2d}\\D_{4h}\end{array}\right.$	4 4/m 422 4mm 42m 4/mmm	2 2 2 2 2 2 2 2 2	4 4 3 3 3 3	4 4 2 2 2 2	2 2 1 1 1 1	0 0 0 0 0 0	0 0 0 0 0 0 0	7 7 6 6 6 6	16 16 12 12 12 12			
Trigonal	$ \left\{\begin{array}{c} C_3\\ C_{3i}\\ D_3\\ C_{3v}\\ D_{3d} \end{array}\right. $	3 3 32 3 <i>m</i> 3 <i>m</i>	2 2 2 2 2	4 3 3 3	8 8 4 4 4	0 0 0 0	0 0 0 0	0 0 0 0 0	7 7 6 6 6	20 20 14 14 14			
Hexagonal	$\left\{\begin{array}{l}C_6\\C_{3h}\\C_{6h}\\D_6\\C_{6v}\\D_{3h}\\D_{6h}\end{array}\right.$	6 6/m 622 6mm Tm2 6/mmm	2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2	4 4 2 2 2 2	2 2 1 1 1 1	2 2 1 1 1 1	2 2 1 1 1 1	5 5 5 5 5 5 5 5	12 12 12 10 10 10 10			
Cubic	$ \left\{\begin{array}{c} T\\ T_h\\ O\\ T_d\\ O_h \end{array}\right. $	23 m3 432 43m m3m	1 1 1 1	2 2 2 2 2	5 5 3 3 3	3 3 2 2 2	2 2 1 1 1	1 1 0 0 0	3 3 3 3 3	8 8 6 6 6			
Isotropic			1	1	1	0	0	0	2	3			

Table 1. Number of elastic constants and number of elements in an integrity basis for each crystal class

Table 2. First, second and third degree anisotropic polynomials and their invariant properties

	Polynomials	Invariance							
1st degree	$\left\{\begin{array}{l}E_{33}\\E_{11}\\E_{31}\end{array}\right.$	Tetragonal, trigonal, hexagonal, orthorhombic, monoclinic Orthorhombic, monoclinic Monoclinic							
2nd degree	$ \begin{cases} E_{12}^2 + E_{23}^2 + E_{31}^2 \\ E_{23}^2 + E_{31}^2 \\ E_{12}(E_{11} - E_{22}) \\ E_{23}(E_{11} - E_{22}) + 2E_{12}E_{31} \\ E_{31}(E_{11} - E_{22}) - 2E_{12}E_{23} \\ E_{23}^2 \\ E_{12}E_{23} \end{cases} $	Tetragonal, cubic Tetragonal, trigonal, hexagonal, orthorhombic, monoclinic Tetragonal (classes 4, $\overline{4}$, $4/m$) Trigonal Trigonal (classes 3, $\overline{3}$) Orthorhombic Monoclinic							
3rd degree	$\begin{cases} E_{11}E_{33}^2 + E_{22}E_{11}^2 + E_{33}E_{22}^2 \\ E_{11}E_{31}^2 + E_{22}E_{12}^2 + E_{33}E_{23}^2 \\ E_{11}E_{22}E_{33} \\ E_{12}E_{23}E_{31} \\ E_{23}E_{31}(E_{11} - E_{22}) \\ E_{12}(E_{23}^2 - E_{31}^2) \\ E_{23}(E_{23}^2 - 3E_{31}^2) \\ E_{23}(E_{11} + E_{22})^2 + 4(E_{12}^2 - E_{22}^2)] + 8E_{11}E_{12}E_{31} \\ E_{31}(E_{31}^2 - 3E_{23}^2) \\ E_{31}[(E_{11} + E_{22})^2 + 4(E_{12}^2 - E_{22}^2)] - 8E_{11}E_{12}E_{23} \\ E_{23}E_{31}(E_{11} - E_{22}) + E_{12}(E_{23}^2 - E_{31}^2) \\ 3E_{12}(E_{11} - E_{22})^2 - 4E_{12}^3 \\ E_{12}(E_{31}^2 - E_{23}^2) + E_{23}E_{31}(E_{22} - E_{33}) \\ E_{11}[(E_{11} + 3E_{22})^2 - 12E_{12}^2] \end{cases}$	Cubic (classes 23, m3) Cubic (classes 23, m3) Cubic Cubic, tetragonal Tetragonal (classes 4, $\overline{4}$, 4/m) Tetragonal (classes 4, $\overline{4}$, 4/m) Trigonal Trigonal (classes 3, $\overline{3}$) Trigonal (classes 6, $\overline{6}$, 6/m) Hexagonal (classes 6, $\overline{6}$, 6/m)							

four and six, as is evidenced from (3), such truncated polynomials of \overline{W} are sufficient for the determination of the second- and third-order elastic constants according to (3). In the following, we shall show the construction of bases in the space of the second-order elastic constants.

To begin with the isotropic integrity basis (2), the second-order elastic constants are obtained from terms of I² and II of (2) in the strain energy \overline{W} . By carrying out the differentiations of (3), one obtains the following two isotropic tensors of rank four,

$$\begin{array}{c} \alpha_{ijkl} = \delta_{ij}\delta_{kl} \\ \beta_{ijkl} = \delta_{ik}\delta_{jl} + \delta_{il}\delta_{jk} \end{array}$$

$$(4)$$

We now introduce the element $(E_{12}^2 + E_{23}^2 + E_{31}^2)$ of Table 2 into the construction of \overline{W} . Differentiation of the term involving this new element in \overline{W} gives the following tensor of rank four which is invariant under the group of transformations characterizing either a cubic or a tetragonal crystal,

$$\pi_{ijkl} = (\delta_{i1}\delta_{j2} + \delta_{i2}\delta_{j1})(\delta_{k1}\delta_{l2} + \delta_{k2}\delta_{l1}) + (\delta_{i2}\delta_{j3} + \delta_{i3}\delta_{j2})(\delta_{k2}\delta_{l3} + \delta_{k3}\delta_{l2}) + (\delta_{i1}\delta_{j3} + \delta_{i3}\delta_{j1})(\delta_{k1}\delta_{l3} + \delta_{k3}\delta_{l1}) .$$
(5)

Consequently, the three elements (α, β, π) of (4) and (5) constitute a tensor basis for the space of the secondorder elastic constants of a cubic crystal. With the additional introduction of the elements E_{33} and $(E_{23}^2 + E_{31}^2)$ of Table 2, the three additional second degree terms E_{33}^2 , $E_{33}(E_{11}+E_{22}+E_{33})$ and $(E_{23}^2+E_{31}^2)$ in \overline{W} produce three more tensors of rank four in addition to (α, β, π) ; they are

$$\left. \begin{array}{l} \gamma_{ijkl} = \delta_{i_3} \delta_{j_3} \delta_{k_3} \delta_{l_3} \\ \delta_{ijkl} = \delta_{ij} \delta_{k_3} \delta_{l_3} + \delta_{i_3} \delta_{j_3} \delta_{kl} \\ \varepsilon_{ijkl} = (\delta_{i_2} \delta_{j_3} + \delta_{i_3} \delta_{j_2}) (\delta_{k_2} \delta_{l_3} + \delta_{k_3} \delta_{l_2}) \\ + (\delta_{i_1} \delta_{j_3} + \delta_{i_3} \delta_{j_1}) (\delta_{k_1} \delta_{l_3} + \delta_{k_3} \delta_{l_1}) . \end{array} \right\}$$
(6)

Therefore, the six elements $(\alpha, \beta, \pi, \gamma, \delta, \varepsilon)$ of (4), (5) and (6) form a basis for the space of the second-order elastic constants of crystals of classes 422, 4mm, $\overline{4}2m$ and 4/mmm in the tetragonal system. At the same time, the five elements $(\alpha, \beta, \gamma, \delta, \varepsilon)$ form a basis for the space of the second-order elastic constants of a hexagonal crystal.

By continuing the computations as outlined above, we obtain sixteen linearly independent tensors of rank four whose expressions are given in Table 3, together with the symmetry classes for which each is an invariant. Table 4 exhibits the use of these tensors to form five hierarchies of bases which span the space of second-order elastic constants for each symmetry class, together with the multiplication tables. The inner product of two tensors A_{ijkl} and B_{ijkl} which enters the multiplication table is defined as $(\mathbf{A}, \mathbf{B}) = A_{ijkl}B_{ijkl}$.

Bases which span the space of elastic constants of orders higher than the second may be computed in a similar manner. The tedious but straightforward algebraic procedures can best be handled by a computer using available symbolic manipulation programming such as FORMAC of 7090/94 IBSYS. In fact, the third-order elastic constants listed by Hearmon (1953) have been reproduced by a FORMAC program but with the additional feature of exhibiting hierarchies of bases similar to Table 4. As the number of the thirdorder elastic constants is so many, as evidenced in Table 1, details of the computer results will not be given here.

3. Orthonormal bases

By a linear combination of elements in a basis in Table 4, one can, instead, construct an orthonormal basis whose elements are (1) mutually orthogonal; *i.e.* $(\mathbf{A}, \mathbf{B}) = 0$, if $A_{ijkl} \neq B_{ijkl}$, and are (2) normal; *i.e.* $(\mathbf{A}, \mathbf{A}) = 1$, for elements A and B in the orthonormal basis. Twenty orthonormal tensors have been constructed. They are displayed in both their tensor forms and their matrix forms in Table 5, together with the

Tab	le	3.	T	ensors	of	rank	'c f	four	and	thei	r i	nvariant	pro	per	tie	?S
-----	----	----	---	--------	----	------	------	------	-----	------	-----	----------	-----	-----	-----	----

***	•
Express	sion

aijki	$=\delta_{ij}\delta_{kl}$	ſ
Bijki	$=\delta_{ik}\delta_{jl}+\delta_{il}\delta_{jk}$	t
π_{ijkl}	$= (\delta_{i1}\delta_{j2} + \delta_{i2}\delta_{j1}) (\delta_{k1}\delta_{l2} + \delta_{k2}\delta_{l1}) + (\delta_{i2}\delta_{j3} + \delta_{i3}\delta_{j2}) (\delta_{k2}\delta_{l3} + \delta_{k3}\delta_{l2})$	Ì
	$+\left(\delta_{i1}\delta_{j3}+\delta_{i3}\delta_{j1} ight)\left(\delta_{k1}\delta_{l3}+\delta_{k3}\delta_{l1} ight)$	
Yijkl	$=\delta_{i3}\delta_{j3}\delta_{k3}\delta_{l3}$	Í
δ_{ijkl}	$=\delta_{ij}\delta_{k3}\delta_{l3}+\delta_{i3}\delta_{j3}\delta_{kl}$	i
Eijkl	$= (\delta_{i2}\delta_{j3} + \delta_{i3}\delta_{j2}) (\delta_{k2}\delta_{l3} + \delta_{k3}\delta_{l2}) + (\delta_{i1}\delta_{j3} + \delta_{i3}\delta_{j1}) (\delta_{k1}\delta_{l3} + \delta_{k3}\delta_{l1})$	l
φ_{ijkl}	$= (\delta_{i1}\delta_{j2} + \delta_{i2}\delta_{j1}) (\delta_{k1}\delta_{l3} + \delta_{k3}\delta_{l1}) + (\delta_{i1}\delta_{j3} + \delta_{i3}\delta_{j1}) (\delta_{k1}\delta_{l2} + \delta_{k2}\delta_{l1})$	
	$+ \left(\delta_{i2}\delta_{j3} + \delta_{i3}\delta_{j2}\right) \left(\delta_{k1}\delta_{l1} - \delta_{k2}\delta_{l2}\right) + \left(K_{i1}\delta_{j1} - \delta_{i2}\delta_{j2}\right) \left(\delta_{k2}\delta_{l3} + \delta_{k3}\delta_{l2}\right)$	
ψ_{ijkl}	$= (\delta_{i1}\delta_{j3} + \delta_{i3}\delta_{j1}) (\delta_{k1}\delta_{l1} - \delta_{k2}\delta_{l2}) + (\delta_{i1}\delta_{j1} - \delta_{i2}\delta_{j2}) (\delta_{k1}\delta_{l3} + \delta_{k3}\delta_{l1})$	
	$-(\delta_{i1}\delta_{j2}+\delta_{i2}\delta_{j1})(\delta_{k2}\delta_{l3}+\delta_{k3}\delta_{l2})-(\delta_{i2}\delta_{j3}+\delta_{i3}\delta_{j2})(\delta_{kl}\delta_{l2}+\delta_{k2}\delta_{l1})$	
ω_{ijkl}	$ = (\delta_{i1}\delta_{j2} + \delta_{i2}\delta_{j1}) (\delta_{k1}\delta_{l1} - \delta_{k2}\delta_{l2}) + (\delta_{i1}\delta_{j1} - \delta_{i2}\delta_{j2}) (\delta_{k1}\delta_{l2} + \delta_{k2}\delta_{l1}) $	
Qijkl	$=\delta_{i1}\delta_{j1}\delta_{k1}\delta_{i1}$	l
θ_{ijkl}	$= (\delta_{i2}\delta_{j3} + \delta_{i3}\delta_{j2}) (\delta_{k2}\delta_{l3} + \delta_{k3}\delta_{l2})$	ł
σ_{ijkl}	$=(\delta_{i3}\delta_{j3}\delta_{k1}\delta_{l1}+\delta_{i1}\delta_{j1}\delta_{k3}\delta_{l3})$	ļ
λijki	$= (\delta_{i2}\delta_{j3} + \delta_{i3}\delta_{j2}) (\delta_{k1}\delta_{l2} + \delta_{k2}\delta_{l1}) + (\delta_{i1}\delta_{j2} + \delta_{i2}\delta_{j1}) (\delta_{k2}\delta_{l3} + \delta_{k3}\delta_{l2})$	l
μ_{ijkl}	$=(\delta_{i1}\delta_{j3}+\delta_{i3}\delta_{j1})\delta_{k3}\delta_{l3}+\delta_{i3}\delta_{j3}(\delta_{k1}\delta_{l3}+\delta_{k3}\delta_{l1})$	ļ
Tijkl	$=(\delta_{i1}\delta_{j3}+\delta_{i3}\delta_{j1})\delta_{k1}\delta_{l1}+\delta_{i1}\delta_{j1}(\delta_{k1}\delta_{l3}+\delta_{k3}\delta_{l1})$	
ζijki	$= (\delta_{i_1}\delta_{j_3} + \delta_{i_3}\delta_{j_1})\delta_{k_2}\delta_{l_2} + \delta_{i_2}\delta_{j_2}(\delta_{k_1}\delta_{l_3} + \delta_{k_3}\delta_{l_1})$	l

Invariance Isotropic Cubic, tetragonal, Orthorhombic, monoclinic

Tetragonal, hexagonal, Trigonal, orthorhombic, Monoclinic

Trigonal Trigonal (classes 3, $\overline{3}$)

Tetragonal (classes $4, \overline{4}, 4/m$)

Orthorhombic, monoclinic

Monoclinic

symmetry classes for which each is an invariant. Table 6 exhibits the five hierarchies of orthonormal tensor bases which span the space of the second-order elastic constants.

Any elastic tensor of rank four possessing certain crystallographic symmetry may be decomposed according to one of the schemes in Table 6. Thus the elastic stiffness tensor of crystals of classes $3,\overline{3}$, for example, can be represented in the form

$$c_{ijkl} = \sum_{K=1}^{\text{VII}} (c, A^K) A_{ijkl}^K, \qquad (7)$$





ť

		Monoclinic Orthorhombic Tetragonal (422, 4mm, 42m, 4/mmm)												
		— Isoti α	ropic $-\beta$	- π	γ	δ	8	Q	σ	θ	x	μ	τ	ζ
(<i>e</i>)	α β π γ δ ε Q σ θ λ μ τ ζ	9	6 24	0 12 12	1 2 0 1	6 4 0 2 8	0 8 8 0 0 8	1 2 0 0 0 0 0 1	2 0 0 2 0 0 2	0 4 4 0 0 4 0 4	0 0 0 0 0 0 0 0 8	0 0 0 0 0 0 0 0 0 0 4	0 0 0 0 0 0 0 0 0 0 0 4	0 0 0 0 0 0 0 0 0 0 0 0 0 4

Table 4 (cont.)

Table 5. Orthonormal tensors of rank four, their matrix representations and their invariant properties

Name	Symmetry	Tensor	Matrix
AI	Isotropic	$A_{ijkl}{}^{\rm I} = \frac{1}{3} \alpha_{ijkl}$	$A_{IJ}^{I} = \frac{1}{3} \left(\begin{array}{ccccccc} 1 & 1 & 1 & 1 & 0 & 0 & 0 \\ 1 & 1 & 1 & 1 & 0 & 0 & 0 \\ 1 & 1 & 1 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0$
A ^{II}	Isotropic	$A_{ijkl}^{II} = \frac{1}{6\gamma5} \left[3\beta_{ijkl} - 2\alpha_{ijkl} \right]$	$A_{IJ}^{II} = \frac{1}{6\sqrt{5}} \begin{pmatrix} 4 & -2 & -2 & 0 & 0 & 0 \\ -2 & 4 & -2 & 0 & 0 & 0 \\ -2 & -2 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 3 & 0 & 0 \\ 0 & 0 & 0 & 0 & 3 & 0 \\ 0 & 0 & 0 & 0 & 0 & 3 \end{pmatrix}$
AC	Cubic Tetragonal Orthorhombic Monoclinic	$A_{ijkl}^{C} = \frac{1}{2l/30} \begin{bmatrix} 5\pi_{ijkl} \\ -3\beta_{ijkl} + 2\alpha_{ijkl} \end{bmatrix}$	$A_{IJ}{}^{C} = \frac{1}{\vec{\gamma}30} \begin{pmatrix} -2 & 1 & 1 & 0 & 0 & 0 \\ 1 & -2 & 1 & 0 & 0 & 0 \\ 1 & 1 & -2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$
A ^{H1}	Tetragonal Hexagonal Trigonal Orthorhombic Monoclinic	$A_{ijkl}{}^{H_1} = \frac{1}{6\sqrt{5}} \begin{bmatrix} 15\gamma_{ijkl} \\ -\beta_{ijkl} - \alpha_{ijkl} \end{bmatrix}$	$A_{IJ}{}^{H_1} = \frac{1}{6\sqrt{5}} \begin{pmatrix} -3 & -1 & -1 & 0 & 0 & 0 \\ -1 & -3 & -1 & 0 & 0 & 0 \\ -1 & -1 & 12 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 & -1 \end{pmatrix}$
<i>А</i> ^{H2}	Tetragonal Hexagonal Trigonal Orthorhombic Monoclinic	$A_{ijkl}^{H2} = \frac{1}{12} [9\delta_{ijkl} - 15\gamma_{ijkl} + \beta_{ijkl} - 5\alpha_{ijkl}]$	$A_{IJ}^{H2} = \frac{1}{12} \begin{pmatrix} -3 & -5 & 4 & 0 & 0 & 0 \\ -5 & -3 & 4 & 0 & 0 & 0 \\ 4 & 4 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$
А ^н 3	Tetragonal Hexagonal Trigonal Orthorhombic Monoclinic	$A_{ijkl}^{H3} = \frac{1}{4} [2\epsilon_{ijkl} - \delta_{ijkl} + 3\gamma_{ijkl} - \beta_{ijkl} + \alpha_{ijkl}]$	$A_{IJ}^{H3} = \frac{1}{4} \begin{pmatrix} -1 & 1 & 0 & 0 & 0 & 0 \\ 1 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0$
A TH	Tetragonal Orthorhombic Monoclinic	$A_{ijkl}{}^{TH} = \frac{1}{2\sqrt{2}} \begin{bmatrix} 2\pi_{ijkl} \\ -\varepsilon_{ijkl} - \delta_{ijkl} + 3\gamma_{ijkl} \\ -\beta_{ijkl} + \alpha_{ijkl} \end{bmatrix}$	$A_{IJ}{}^{TH} = \frac{1}{2\sqrt{2}} \begin{pmatrix} -1 & 1 & 0 & 0 & 0 & 0 \\ 1 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0$

Name	Symmetry classes	Tensor	Matrix
A ^{TC1}	Tetragonal Orthorhombic Monoclinic	$A_{ijkl}{}^{TC1} = \frac{1}{\sqrt{6}} \left[3\gamma_{ijkl} + \frac{1}{2}\pi_{ijkl} - \frac{1}{2}\beta_{ijkl} \right]$	$A_{IJ}{}^{TC1} = \frac{1}{l'6} \begin{pmatrix} -1 & 0 & 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0$
A ^{TC2}	Tetragonal Orthorhombic Monoclinic	$A_{ijkl}{}^{TC2} = \frac{1}{2l/3} \begin{bmatrix} 3\delta_{ijkl} \\ -6\gamma_{ijkl} - \pi_{ijkl} \\ +\beta_{ijkl} - 2\alpha_{ijkl} \end{bmatrix}$	$A_{IJ}{}^{TC2} = \frac{1}{2\gamma3} \begin{pmatrix} 0 & -2 & 1 & 0 & 0 & 0 \\ -2 & 0 & 1 & 0 & 0 & 0 \\ 1 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0$
A ^{TC3}	Tetragonal Orthorhombic Monoclinic	$A_{ijkl}{}^{TC3} = \frac{1}{2l/6} \left[3\varepsilon_{ijkl} - 2\pi_{ijkl} \right]$	$A_{IJ}{}^{TC3} = \frac{1}{2\nu6} \left(\begin{array}{ccccccc} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 &$
ATET	Tetragonal (classes 4,4,4/m)	$A_{ijkl}{}^{TET} = \frac{1}{2/2} \omega_{ijkl}$	$A_{IJ}{}^{TET} = \frac{1}{2\gamma 2} \left(\begin{array}{cccccc} 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0$
A ^{TR1}	Trigonal	$A_{ijkl}^{TR1} = \frac{1}{4}\varphi_{ijkl}$	$A_{IJ}{}^{TR_1} = \frac{1}{4} \left(\begin{array}{cccccccc} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 1 & 0 \end{array} \right)$
A ^{TR2}	Trigonal (classes $3, \overline{3}$)	$A_{ijkl}{}^{TR2} = \frac{1}{4} \psi_{ijkl}$	$A_{IJ}{}^{TR2} = \frac{1}{4} \left(\begin{array}{cccccc} 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0$
A ^{VII}	Orthorhombic Monoclinic	$A_{ijkl}^{\text{VII}} = \frac{1}{\sqrt{2}} \left[2\varrho_{ljkl} + \frac{1}{2} \pi_{ijkl} + \gamma_{ijkl} - \frac{1}{2} \beta_{ijkl} \right]$	$A_{IJ}^{\text{VII}} = \frac{1}{\sqrt{2}} \left(\begin{array}{ccccccc} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0$
A ^{VIII}	Orthorhombic Monoclinic	$A_{ijkl}^{\text{VIII}} = \frac{1}{2} [2\sigma_{ijkl} \\ -\delta_{ijkl} + 2\gamma_{ijkl}]$	$A_{IJ}^{\text{VIII}} = \frac{1}{2} \left(\begin{array}{ccccccc} 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 & 0 & 0 \\ 1 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0$
AIX	Orthorhombic Monoclinic	$A_{ijkl}^{\mathrm{IX}} = \frac{1}{2l/2} \left[2\theta_{ijkl} - \varepsilon_{ijkl} \right]$	$A_{IJ}^{IX} = \frac{1}{2\sqrt{2}} \left(\begin{array}{ccccccc} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 &$
AX	Monoclinic	$A_{ijkl} \mathbf{x} = \frac{1}{2\sqrt{2}} \lambda_{ijkl}$	$A_{IJ}{}^{\mathrm{X}} = \frac{1}{2 \not\!$

Name	Symmetry classes	Tensor		Mat	rix				
A ^{XI}	Monoclinic	$A_{ijkl}^{XI} = \frac{1}{2}\mu_{ijkl}$	$A_{IJ}^{XI} = \frac{1}{2} \left(\right)$	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 1 0	0 0 0 0 0	0 0 1 0 0 0	0 0 0 0 0 0	$\Big)$
A ^{XII}	Monoclinic	$A_{ijkl}^{\rm XII} = \frac{1}{2} \tau_{ijkl}$	$A_{IJ}^{XII} = \frac{1}{2}$	0 0 0 0 0 0 0 0 0 0 0 0 0 1		0 0 0 0 0 0	1 0 0 0 0	0 0 0 0 0 0	$\Big)$
A ^{XIII}	Monoclinic	$A_{ijkl}^{\rm XIII} = \frac{1}{2} \zeta_{ijkl}$	$A_{IJ}^{XIII} = \frac{1}{2}$	0 0 0 0 0 0 0 0 0 1 0 0	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0	0 1 0 0 0	0 0 0 0 0	$\Big)$

Table 5 (cont.)

Table 6. Five hierarchies of orthonormal bases

	A^{I}	A^{II}	A^{III}	A^{IV}	A ^v	A^{VI}	A^{VII}	$A^{\rm VIII}$	A^{IX}	A ^x	A^{XI}	A^{XII}	A^{XIII}	
(a)	A ^I — Isotroj 	A ¹¹ pic — — H — Tri	A ^{H1} exagon	A^{H_2} al	A^{H_3}	A ^{TR1}	A^{TR2}	1						
			T	rigonal	(3,3)			-						
(b)	A ^I — Isotro	A ^{II} pic	AC	A^{TC1}	A^{TC2}	A ^{TC3}	A^{TET}							
	—— Te	tragon	al (422 – Tetr	,4 <i>mm</i> ,42 agonal (2 <i>m</i> ,4/ <i>mm</i> [4, 4 ,4/ <i>m</i>)	m) ——								
(c)	Tetr	A ^{II} pic —! —— H ragona	A ^{H1} lexagon l (422,4 - Tetrag	A^{H_2} al	A^{H3} $n, 4/mmn$ $\overline{4, 4/m}$	A TH	ATET							
(<i>d</i>)	— Isotro — Tetr	A ¹¹ pic — H ragona	A ^{H1} [exagon [(422, 4	A^{H_2} al $$	A ^{H3} n,4/mmn	A^{TH}	A ^{VII}	A ^{VIII}	A ^{IX} !	A ^x	A ^{XI}	A ^{XII}	AXIII	
							- Mono	clinic —						· · ·
(e)	— Isotro	A ^{II} pic — Cubic-		A^{TC1}	ATC2	A ^{TC3}	A^{VII}	A ^{VIII}	AIX	A ^x	A ^{XI}	A ^{XII}	AXIII	
	1e	tragon	ai (422	,4 <i>mm</i> ,42 —— C	2 <i>m</i> , 4/ <i>mm</i> Prthorhor	<i>m)</i> nbic			ii					
							– Mono	clinic —						

where A^{K} , K=I, II, ..., VII are the orthonormal basis according to Table 6 (a), and (c, A^{K}) is the inner product of c_{ijkl} and A^{k}_{ijkl} . Likewise, the elastic stiffness tensor of classes 4,4 and 4/m crystals may be represented in the same form as (7) but with A^{K} chosen to be the orthonormal basis according to either (b) or (c) of Table 6.

In order to facilitate the computation of inner products of an arbitrary elastic stiffness tensor c_{ijkl} and an element of an orthonormal basis, Table 7 lists the

 Table 7. Formulas for the computation of inner products in terms of matrix elements

$$\begin{split} S_1 &= \sum_{I=1}^{3} c_{II}, \quad S_2 &= \sum_{I=4}^{6} s_{II}, \quad S_3 &= \sum_{I=1}^{3} \sum_{I=1}^{3} c_{IJ} \\ I &= 1 \quad J = 1 \\ (c, A^{I}) &= \frac{1}{3}S_3 \\ (c, A^{II}) &= \frac{1}{3\sqrt{5}} \left[3S_1 + 6S_2 - S_3 \right] \\ (c, A^{C}) &= \frac{1}{\sqrt{30}} \left[4S_2 - 3S_1 + S_3 \right] \\ (c, A^{H1}) &= \frac{1}{6\sqrt{5}} \left[15c_{33} - 2S_1 - 4S_2 - S_3 \right] \\ (c, A^{H2}) &= \frac{1}{12} \left[18(c_{13} + c_{23}) + 3c_{33} + 2S_1 + 4S_2 - 5S_3 \right] \\ (c, A^{H3}) &= \frac{1}{4} \left[8(c_{44} + c_{55}) - 2(c_{13} + c_{23}) + c_{33} - 2S_1 - 4S_2 + S_3 \right] \\ (c, A^{TH}) &= \frac{1}{2\sqrt{2}} \left[4c_{66} - 2(c_{13} + 2c_{23}) + c_{33} - 2S_1 + S_3 \right] \\ (c, A^{TC1}) &= \frac{1}{\sqrt{6}} \left[3c_{33} - S_1 \right] \end{split}$$

formulas in terms of matrix elements c_{IJ} , I, J = 1, 2, ..., 6. However, for the elastic compliance tensor s_{ijkl} , the coefficients in the formulas must be divided by 2 when either I or J of s_{IJ} is 4, 5, 6 and by 4 when both I and J of s_{IJ} are 4, 5 or 6.

$$c_{IJ} = \begin{pmatrix} 8.680 & 0.704 & 1.191 \\ 0.704 & 8.680 & 1.191 \\ 1.191 & 1.191 & 10.575 \\ -1.804 & 1.804 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

We now define and denote the norm of c_{ijkl} by

$$|c|| = \{c_{ijkl} \, . \, c_{ijkl}\}^{\frac{1}{2}} \, . \tag{8}$$

When c_{ijkl} is in the space spanned by the orthonormal basis $\{A^K\}$, it is easy to see that

$$||c|| = \{\sum_{K} (c, A^{K})\}^{\frac{1}{2}}.$$
 (9)

The nearest isotropic tensor, denoted by c_{ijkl}^{0} , of c_{ijkl} is therefore

$$c_{ijkl}^{0} = \sum_{K=1}^{L} (c, A^{K}) A_{ijkl}^{K}$$
(10)

$$c_{IJ} = \begin{pmatrix} 10.250 & 2.726 & -0.803\\ 2.726 & 8.680 & -0.831\\ -0.803 & -0.831 & 12.992\\ 0 & 0 & 0\\ -0.929 & 0.388 & -0.577\\ 0 & 0 & 0 \end{pmatrix}$$

which has a norm

$$||c^{0}|| = \left\{ \sum_{K=1}^{\Pi} (c^{0}, A^{K}) \right\}^{\frac{1}{2}}.$$
 (11)

In a similar manner, with respect to the tensor c_{ijkl} , the nearest tensors of other symmetry classes within the class spanned by the basis $\{A^K\}$ may be read off readily from the representation, and their norms may be computed according to (9).

$$S_{1} = \sum_{I=1}^{3} c_{II} , \quad S_{2} = \sum_{I=4}^{6} s_{II} , \quad S_{3} = \sum_{I=1}^{3} \sum_{J=1}^{3} c_{IJ}$$

$$(c, A^{TC2}) = \frac{1}{|J|} [3(c_{13} + c_{23}) + S_{1} - S_{3}]$$

$$(c, A^{TC3}) = |J/2/3[c_{44} + c_{55} - 2c_{66}]$$

$$(c, A^{TR1}) = 2c_{56} + c_{14} - c_{24}$$

$$(c, A^{TR2}) = c_{15} - c_{25} - 2c_{46}$$

$$(c, A^{VII}) = \frac{1}{|J|} [c_{11} - c_{22}]$$

$$(c, A^{XI}) = |J|^{2} [c_{44} - c_{55}]$$

$$(c, A^{XI}) = 2J^{2} c_{45}$$

$$(c, A^{XII}) = 2J^{2} c_{45}$$

$$(c, A^{XIII}) = 2c_{15}$$

$$(c, A^{XIII}) = 2c_{15}$$

$$(c, A^{XIII}) = 2c_{15}$$

$$(c, A^{XIII}) = 2c_{15}$$

$$(c, A^{XIII}) = 2c_{25}$$

4. Example

According to McSkimin, Andreatch & Thurston (1965), the elastic stiffness matrix c_{IJ} at room temperature of quartz (class 32) is given by

$$\begin{array}{cccc} -1\cdot804 & 0 & 0 \\ 1\cdot804 & 0 & 0 \\ 0 & 0 & 0 \\ 5\cdot820 & 0 & 0 \\ 0 & 5\cdot820 & -1\cdot804 \\ 0 & -1\cdot804 & 3\cdot988 \end{array}$$
 (12)

in 10^{11} dyn.cm⁻². Using scheme (a) of Table 6, the above matrix may be represented in the form

$$c_{IJ} = 11 \cdot 368A^{\mathrm{I}} + 21 \cdot 386A^{\mathrm{II}} + 0.457A^{H_1} + 1 \cdot 870A^{H_2} + 3 \cdot 663A^{H_3} - 7 \cdot 216A^{TR_1}.$$
(13)

For an AT-cut quartz plate (yxl) 35°, if we orient the Cartesian coordinates in such a way that the (x_1, x_2) plane lies on the middle plane of the plate and $x_2||x$, the matrix (12), referred to the new coordinates, becomes

$$\begin{pmatrix} 0 & -0.929 & 0 \\ 0 & 0.388 & 0 \\ 0 & -0.577 & 0 \\ 2.895 & 0 & -0.243 \\ 0 & 3.825 & 0 \\ .0.243 & 0 & 6.912 \end{pmatrix}$$
(14)

which possesses the symmetry of the monoclinic system. This matrix may be represented in either of the following two ways according to scheme (d) or (e) of Table 6.

$$c_{IJ} = 11 \cdot 368A^{1} + 21 \cdot 386A^{11} + \begin{cases} 3 \cdot 160A^{H1} - 3 \cdot 549A^{H2} - 3 \cdot 560A^{H3} + 5 \cdot 010A^{TH} \\ -1 \cdot 301A^{C} + 2 \cdot 880A^{TC1} - 4 \cdot 091A^{TC2} - 5 \cdot 800A^{TC3} \end{cases} + 1 \cdot 110A^{VII} + 0 \cdot 027A^{VIII} - 1 \cdot 315A^{IX} - 0 \cdot 689A^{X} \\ -1 \cdot 155A^{XI} - 1 \cdot 859A^{XII} + 0 \cdot 776A^{XIII} \end{cases}$$
(15)

The nearest tensors of higher symmetry may be read off from equations (13) or (15). In particular, the nearest isotropic tensor, c_{ijkl}^0 , being an invariant, has the following matrix:

in a perturbation scheme of plane stress problems in anisotropic theory of elasticity.

The author is indebted to Dr R.A.Toupin for his criticism and help.

$$c_{IJ}^{0} = \begin{pmatrix} 10.165 & 0.601 & 0.601 & 0 & 0 & 0\\ 0.601 & 10.165 & 0.601 & 0 & 0 & 0\\ 0.601 & 0.601 & 10.165 & 0 & 0 & 0\\ 0 & 0 & 0 & 4.782 & 0 & 0\\ 0 & 0 & 0 & 0 & 4.782 & 0\\ 0 & 0 & 0 & 0 & 0 & 4.782 \end{pmatrix}.$$

$$(16)$$

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Define the number ε^0 by

$$\varepsilon^{0} = \frac{||c|| - ||c^{0}||}{||c||}.$$
 (17)

 ε^{0} is a scalar constant independent of the rotation of the axes. It is a measure of 'nearness' of the nearest isotropic tensor. The value of ε^{0} for quartz at roomtemperature is found to be 0.054. The use of ε^{0} as a perturbation parameter is currently being investigated

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The Atomic Mechanism of the Body-Centred Cubic to σ -Phase Transformation

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An atomic mechanism for the body-centred cubic to σ -phase transformation is suggested. Atomic movements over small distances in the $[11T]_{b.e.e.}$ direction take place leading to the formation of a new layer structure. The transformation is completed by rotation of alternate layers of hexagons within zones related to kagomé tile structures. The mechanism suggests that certain groups of atoms are more strongly bonded in the [11T] direction than others. The mechanism also suggests that the body-centred cubic phase exhibits partial long range order prior to the transformation. The ductility of β -uranium and the brittleness of FeCr and 2NbA1 alloys is discussed in terms of the ordering and coordination numbers of the atomic positions in the σ structure.

Introduction

The occurrence of the σ phase and its properties have been reviewed by Hall & Algie (1966). The σ phase

always contains at least one transition group element. In alloys it is one of a series of phases occurring with the passage from the more open body-centred cubic structure to the closer packed hexagonal and face-







Fig. 1. The σ -phase structure described as a layer structure of kagomé tiles and diamond nets. The outline of the unit cell is also shown.